

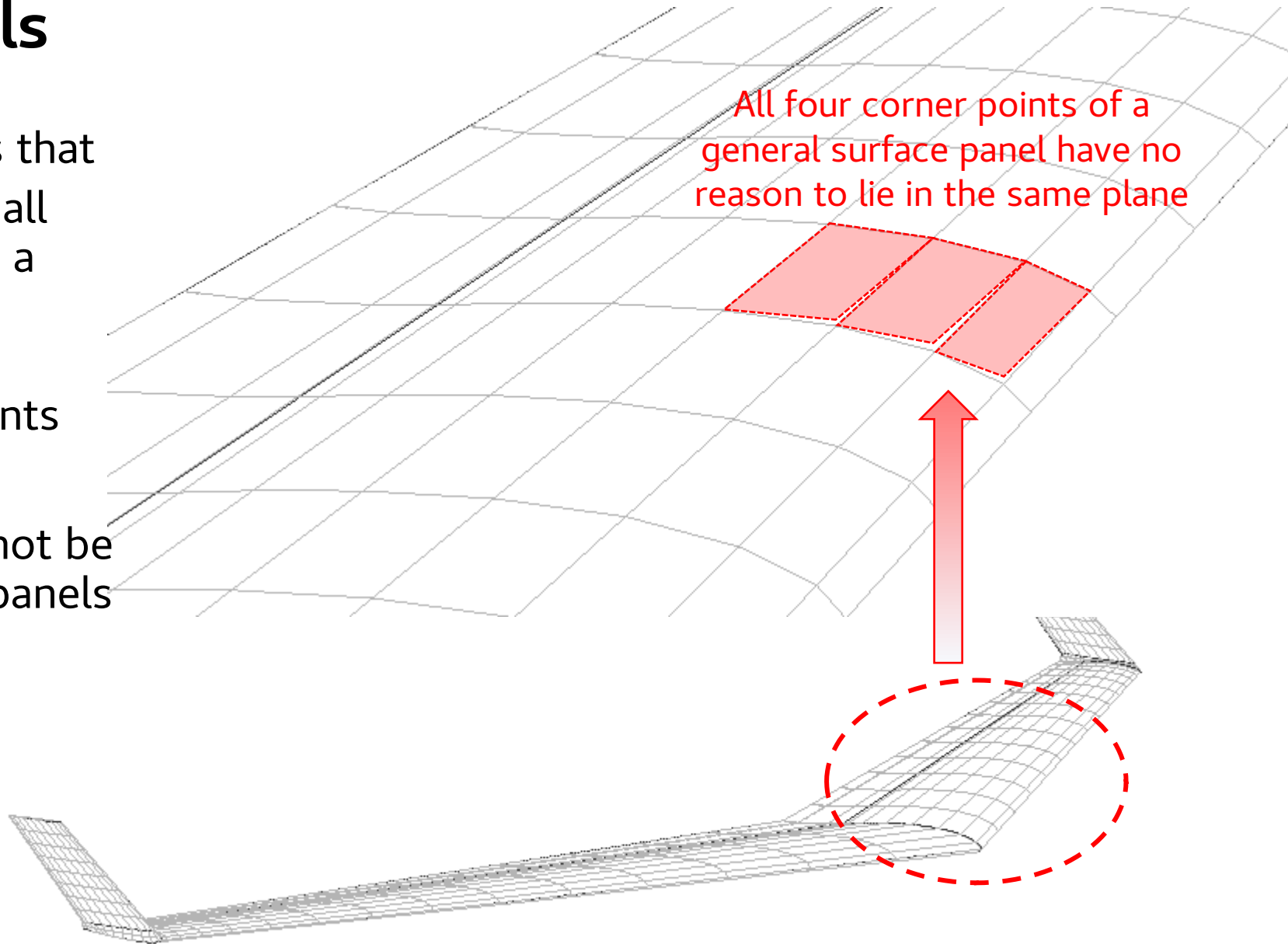
# Triangle-based Galerkin panel methods

# Motivation

- Lift the two restrictions associated to xflr5's quad panels method
  - (1) Impossibility to cover general 3d surfaces with flat quad panels
  - (2) Limited to uniform source and doublet densities
- A triangle-based method is necessary to model fuselage-wings connections.

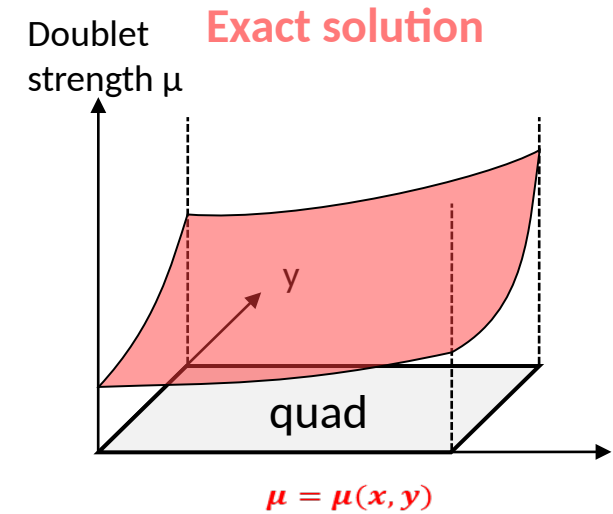
# (1) Flat quad panels

- The 3d panel method requires that
  - (1) quad panels are flat, i.e. all four corner points are in a plane
  - (2) the volumes are entirely closed by surface elements
- However
  - 3d surfaces generally cannot be decomposed in flat quad panels

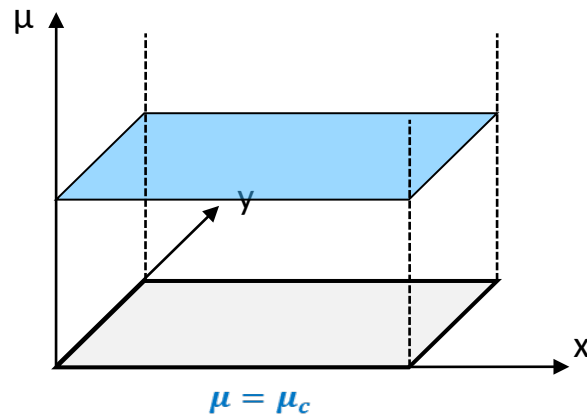


## (2) Uniform strength singularities

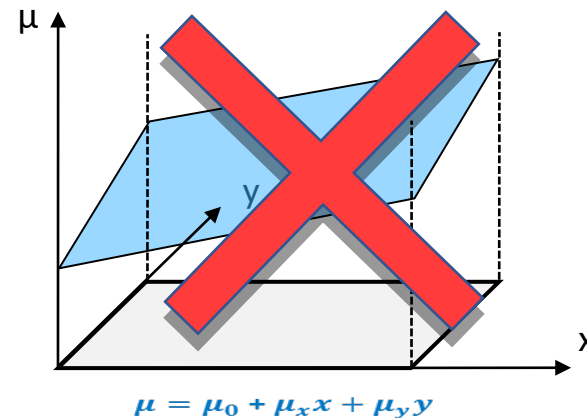
- Panels method in xflr5 are of the uniform type
  - Uniform vortex strength on each panel in the case of the VLM
  - Uniform source and doublet strengths in the case of the panel method
- Methods of higher order are more precise



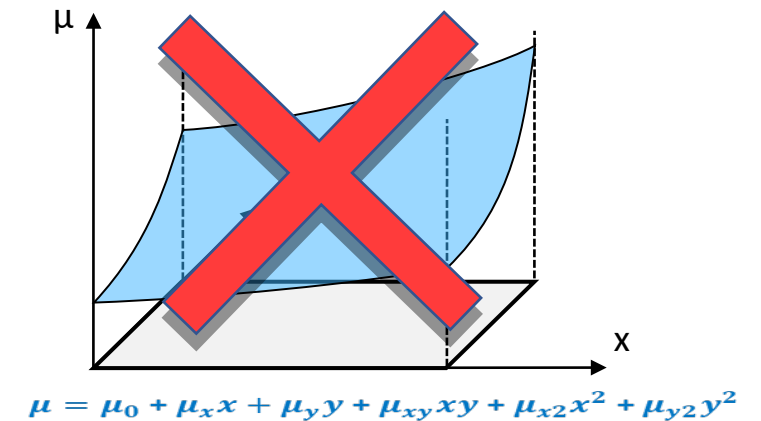
Uniform model  
order 0



Linear model  
order 1

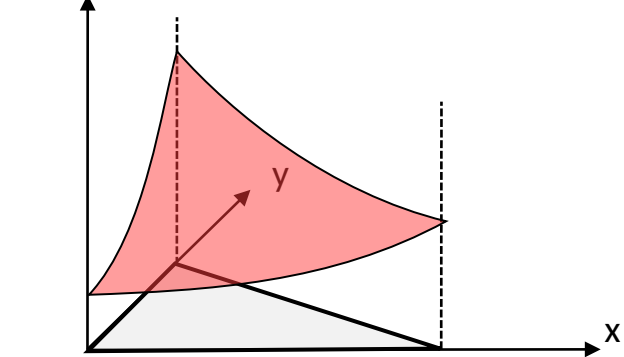


Quadratic model  
order 2



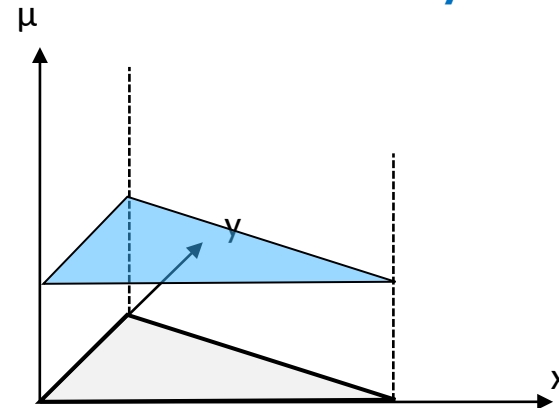
# A triangular Galerkin method solves all three issues

Doublet strength  $\mu$  **Exact solution**



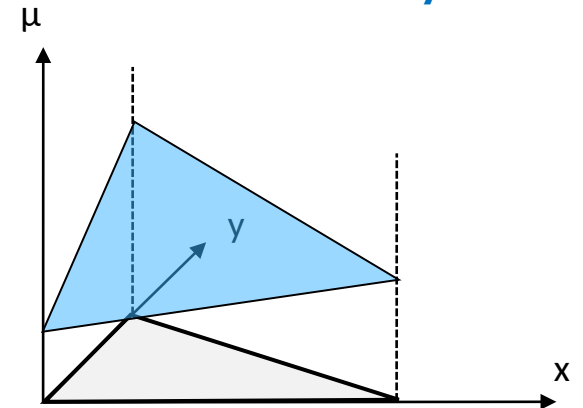
$$\mu = \mu(x, y)$$

**Uniform density**

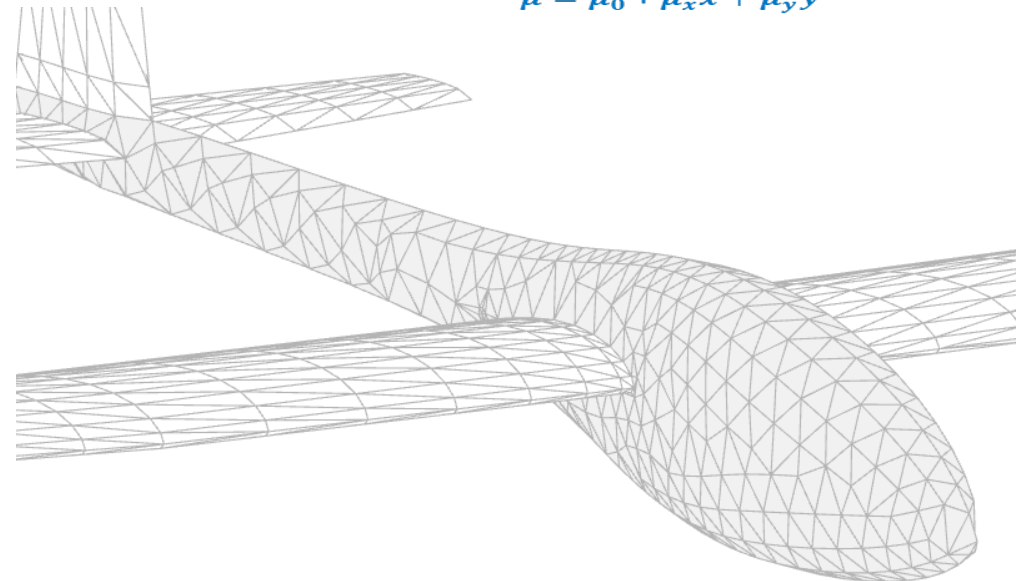
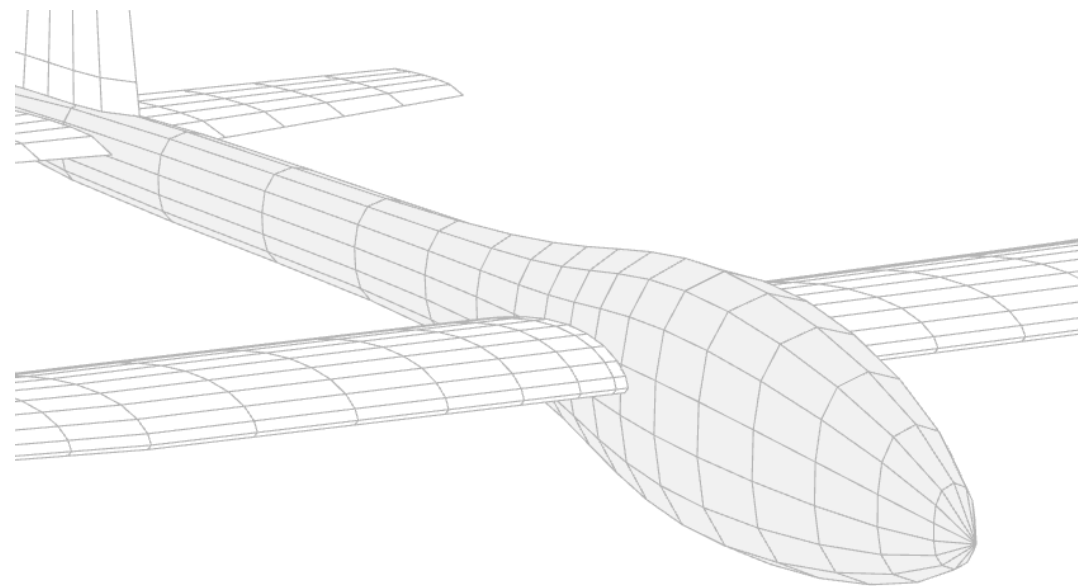


$$\mu = \mu_c$$

**Linear density**



$$\mu = \mu_0 + \mu_x x + \mu_y y$$



# About the triangular methods in flow5

1. flow5 replaces each quad panel with two triangles



Twice as many elements

2. The linear method uses 3 degrees of freedom (d.o.f.) for each triangle instead of 1 d.o.f. for the uniform method

- The linear system for the linear method is 3x the size that of the uniform method
- The LU decomposition time of the system's matrix increases as  $\frac{2}{3} n^3$



Not an issue with the super-powerful Intel<sup>®</sup> MKL library

## About the triangular methods in flow5 (cont.)

3. Matrices used in Boundary Element Methods (BEM) are dense and not sparse like in F.E. analysis  
⇒ memory footprint increases as  $n^2$



Matrix sizes up to 15k x 15k are possible on a 8GB PC

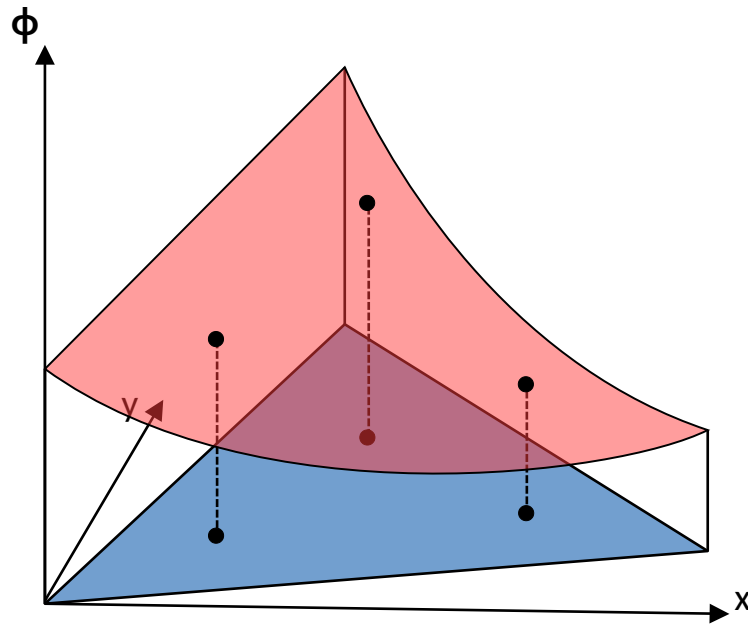
4. The linear method requires the evaluation of surface integrals.



Matrix and RHS construction times are longer than for uniform methods

# About the triangular methods in flow5 (cont.)

- The linear method involves the calculation of surface integrals on the triangles
- These integrals are performed using Gaussian quadrature
- The greater the number of quadrature points, the better the precision.
- The times to construct the influence matrix and the RHS vectors will increase proportionally to  $n_q$



**Order 2 → 3 quadrature points**

Order 1:	1 quadrature point
Order 2:	3 quadrature points
Order 3:	4 quadrature points
Order 4:	6 quadrature points
Order 5:	7 quadrature points
Order 6:	12 quadrature points
Order 7:	13 quadrature points
Order 8:	16 quadrature points
<b>Recommendation:</b>	$3 \leq \text{order} \leq 5$



## About the triangular methods in flow5 (cont.)

5. Galerkin methods can be used with mixed Dirichlet and Neumann BC



Wings can be modelled either as thick Dirichlet volumes or thin Neumann surfaces

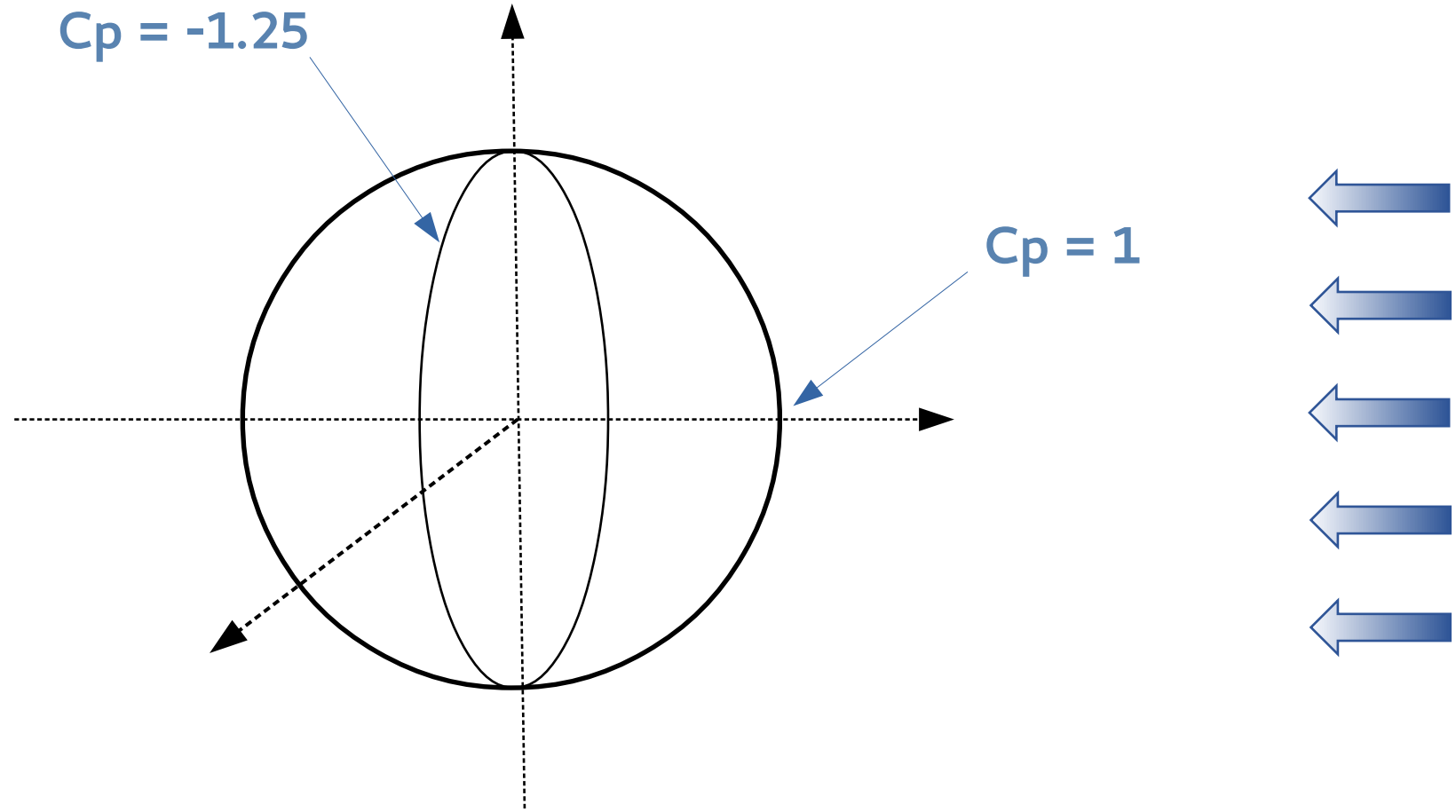
6. Higher order methods are usually recommended over low order methods



Prefer the uniform method for the preliminary design and the linear method in the final stages of the design

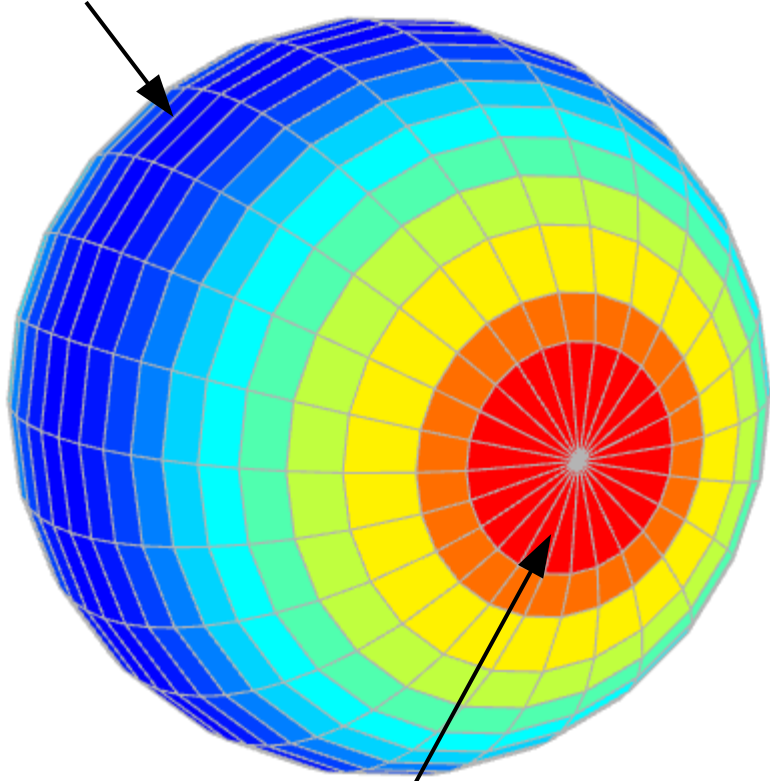
# Pressure coefficients

Theoretical solution for the sphere in a potential flow



# Pressure coefficients - « iso quad-mesh »

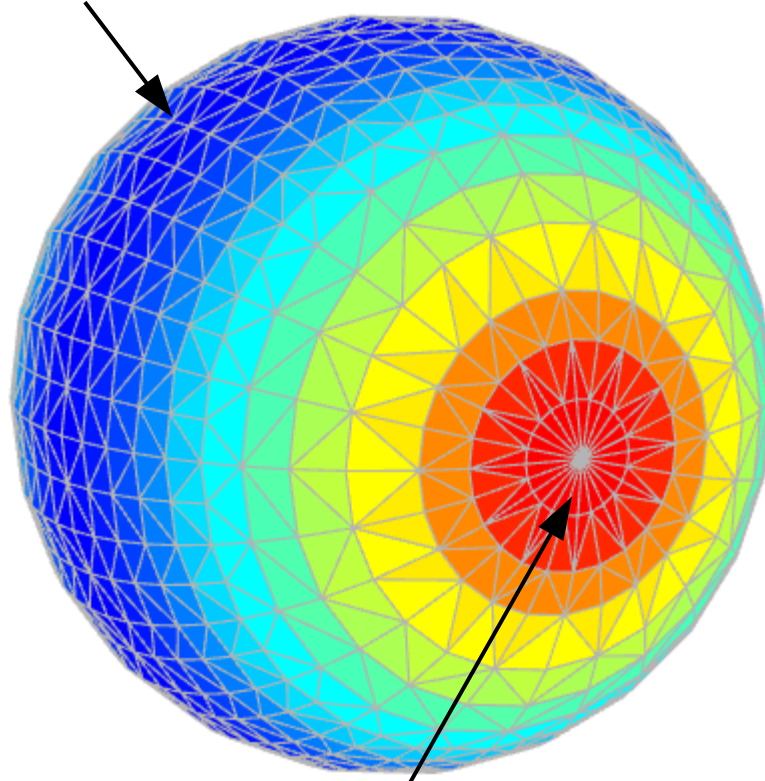
$C_p = -1.24$



$C_p = 0.91$

Uniform quads

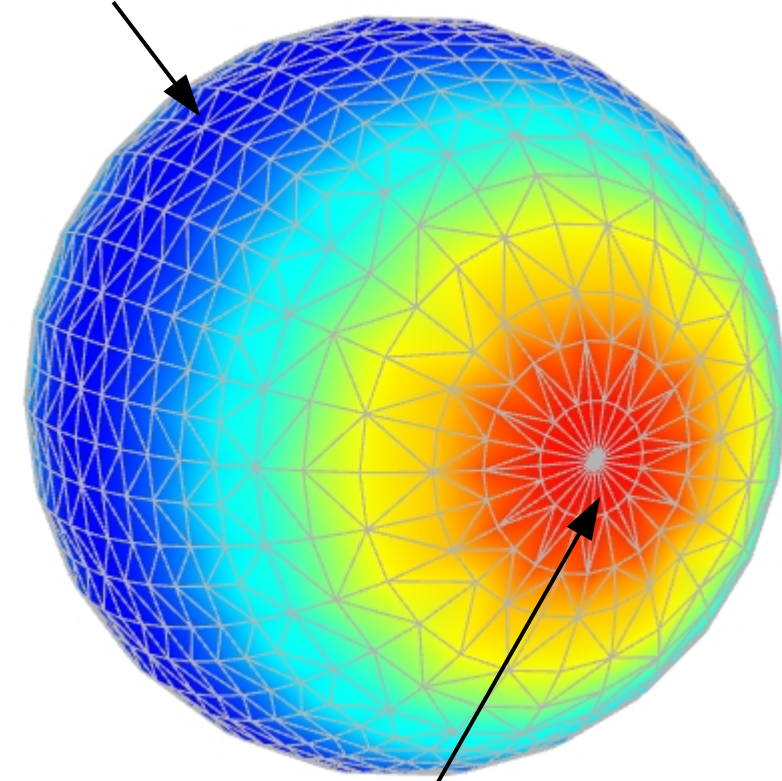
$C_p = -1.26$



$C_p = 0.95$

Uniform triangles

$C_p = -1.18$



$C_p = 0.98$

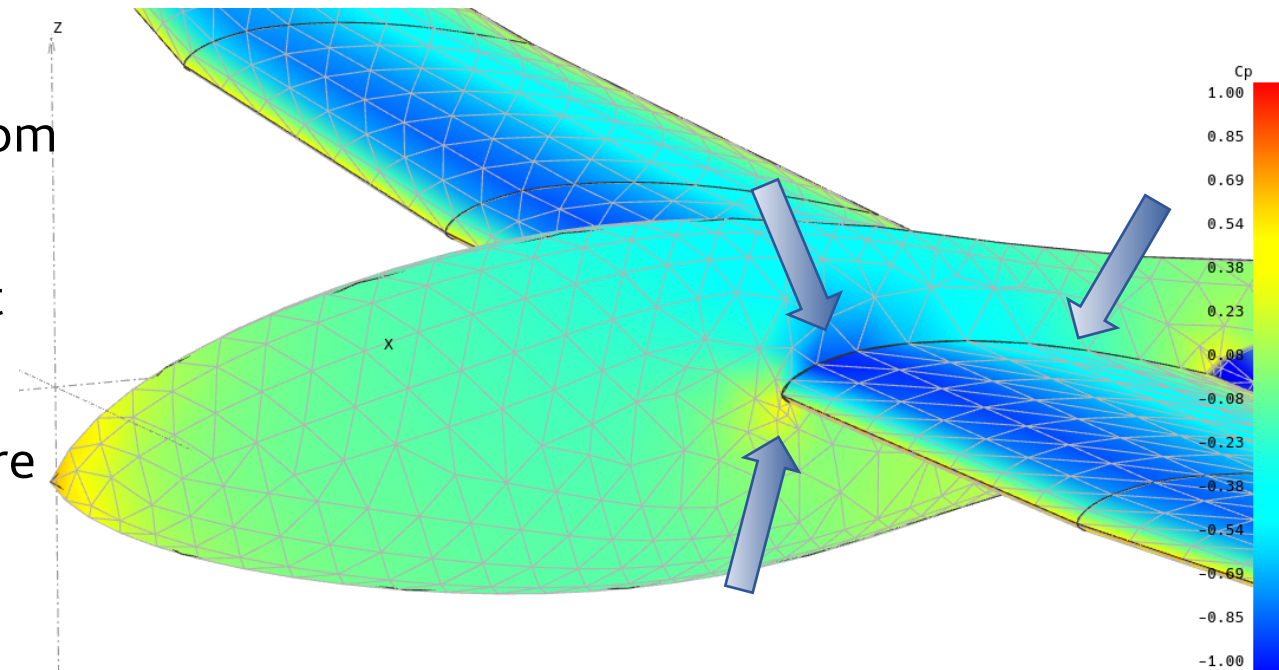
Linear triangles

Not as precise in the area of high gradient

Potential for improvement

# Pressure coefficients - $C_p$

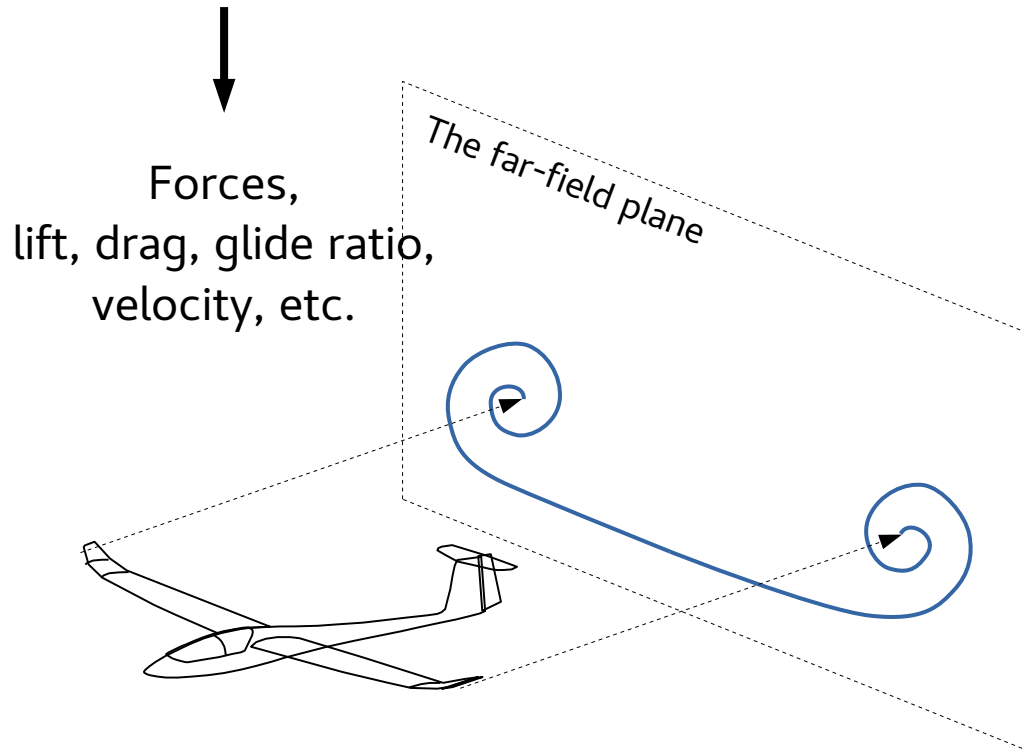
- The pressure coefficients ( $C_p$ ) are calculated from the surface gradient of the doublet densities.
- This requires that the elements be connected at their nodes
- The calculation is tricky when adjacent panels are not in the same plane such as at the junction of wings and fuselages
- It only impacts the moments which are calculated from pressure forces acting on the panels.
- It does not impact the lift and drag calculated in the far-field plane
- Potential to improve the precision of the  $C_p$  coefficients in the linear case  
→ to be evaluated in the  $\beta$ -phase



# Doublet densities

A panel analysis solves the linear system for the doublet densities on the panels. All other results are deduced from the doublet densities.

“Off-body” results calculated downstream in the far-field plane



“On-body” results calculated on the surfaces

Surface gradient of the doublet density

Pressure coefficients, panel forces, moments

